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This is an **author produced version** of a paper published in:

International Journal of Computer Vision 124.3 (2017): 273 – 286

**DOI:** <http://dx.doi.org/10.1007/s11263-017-1024-8>

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# A Closed-form Focus Profile Model for Conventional Digital Cameras

## Supplemental material

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### 1 Sampling and quantization

This section describes in more detail the steps that take place in the digitization of an image: sampling and quantization.

#### 1.1 Sampling

In the process of sampling, a continuous 2D irradiance field  $I_c(x_c, y_c)$  is mapped to a discrete 2D image,  $I(x, y)$ . In this document,  $x$  and  $y$  are discrete spatial variables, whereas the sub-index  $c$  has been used to indicate continuity in the space domain. With this notation, the sampling of the continuous signal  $I_c(x_c, y_c)$  into its discrete counterpart can be described as [34]:

$$I_c(x_c, y_c) \rightarrow I(x, y) = I_c(mS_x, nS_y), \quad (1)$$

where  $S_x$  and  $S_y$  are the sample spacings, in the  $x$  and  $y$  directions, respectively;  $m = \{1, 2, \dots, M\}$  and  $n = \{1, 2, \dots, N\}$  are the discrete image indices, assuming that the discrete 2D image has  $M \times N$  samples.

The sampling rule in (1) is an ideal representation that takes samples of the continuous image irradiance on infinitesimal 2D spots at coordinates  $(mS_x, nS_y)$ . However, in practice, the sensing device relies on processing a small area of finite size in order to estimate the energy of the irradiance corresponding to a single location. Specifically, each pixel consists of a photosensor aimed at measuring the image irradiance by integrating it both in the spatial and temporal domains. For illustration purposes, let us consider the simplest case of an individual imaging sensor consisting of a matrix of squared photoreceptors (see Fig. 1). In this case, the image irradiance is integrated over the area of each individual photoreceptor. Thus, the sample at coordinates  $(x, y)$  corresponds to [12]:

$$I(x, y) = G\beta\lambda \frac{\tau}{hc} \int \int_{\Omega(x_c, y_c)} I(x_c, y_c) dx_c dy_c, \quad (2)$$

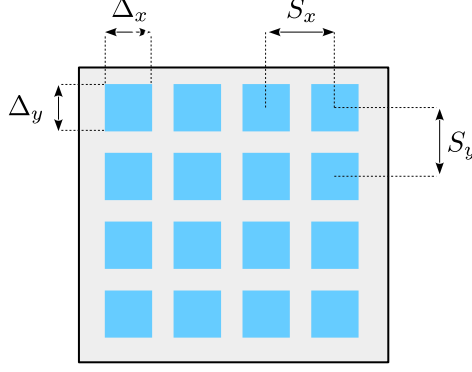


Figure 1: Image sampling.  $\Delta_x \times \Delta_y$  is the detector size and  $S_x$  and  $S_y$  are the sample spacings in the horizontal and vertical directions, respectively.

where  $\Omega(x_c, y_c)$  is a neighborhood that covers the  $\Delta_x \times \Delta_y$  pixel area so that  $\Omega(x_c, y_c) = \{(x, y) | x \in [x_c - 0.5\Delta_x, x_c + 0.5\Delta_x] \wedge y \in [y_c - 0.5\Delta_y, y_c + 0.5\Delta_y]\}$ ,  $G$  is the sensor gain constant,  $\beta$  is the quantum efficiency of the photosensor (the conversion rate between incoming photons and unit charges),  $\lambda$  is the wavelength of the incoming light,  $\tau$  is the integration time (exposure) and  $h$  and  $c$  are the Plank's constant and the speed of light, respectively <sup>1</sup>.

The effect of integrating over a finite spot in (2) combined with the sampling of (1), can be interpreted as applying an averaging filter and the multiplication with an impulse train [9]:

$$I(x, y) = I(x_c, y_c) * A(x_c, y_c) \sum_{m=1}^M \sum_{n=1}^N \delta(x_c - nS_x, y_c - mS_y), \quad (3)$$

where  $A(x_c, y_c)$  is a bi-dimensional squared window of size  $\Delta_x \times \Delta_y$  and  $\delta(x_c, y_c)$  is the impulse function.

By simple inspection of the convolution in (3), it is clear that the image irradiance is low-pass filtered by the sampling spot. Thus, the sampling spot may be utilized to perform pre-sampling filtering for avoiding aliasing. Aliasing is an undesired effect that can appear when representing a continuous domain function with a discrete number of samples. Specifically, according to the Nyquist-Shannon sampling theorem, the continuous domain irradiance,  $I_c$ , must be band-limited in order to avoid *aliasing* [10]:

$$\xi_c < \frac{1}{2S_x}, \quad \eta_c < \frac{1}{2S_y}, \quad (4)$$

<sup>1</sup>Strictly, the quantum efficiency is a function of the wavelength:  $\beta = f(\lambda)$ . Therefore, in polychromatic illumination, (2) involves an integral as a function of  $\lambda$  [12]. For simplicity, this step has been omitted since it is not essential for the subsequent discussion.

where  $\xi_c$  and  $\eta_c$  are the cut-off frequencies of  $I_c$  in the  $x$  and  $y$  directions, respectively.

Bearing the previous discussion in mind, the selection of the sampling steps,  $S_x$  and  $S_y$ , as well as the dimension of the sampling spot,  $\Delta_x \times \Delta_y$  is an important design criterion that determines the final resolution of the imaging system [25]. It is important to remark that, even in perfect focus, the imaged target is blurred due to the effect of diffraction. This diffraction blurring can be interpreted as a band-limiting effect of the system's optics. As a result, in order to optimize the acquisition process, the sensor resolution must be designed to be as close as possible to the resolution of the system's optics at the diffraction limit [5].

## 1.2 Quantization

During sampling, photodetectors work as transducers that convert the image irradiance into electric charge. In conventional cameras, the output of the detector is then amplified and converted to a discrete value. For instance, in 8-bit monochromatic images (gray-scale images), each pixel is assigned a value between 0 and 255 according to the measured irradiance, being 255 the maximum allowed brightness and 0 the minimum one. Quantization is the process of scaling and discretizing the measured values. Both, photodetector measurement and quantization imply the addition of different noise types to the ideal sensed image. For instance, a CCD camera has several primary noise sources, such as *fixed pattern noise*, *dark current noise*, *shot noise*, *amplifier noise* and *quantization noise* [11], which can be grouped into both irradiance-dependent and irradiance-independent sources. In that way, a noisy image  $I_n$  can be modeled as [17]:

$$I_n = g(I + n_s + n_c) + n_q, \quad (5)$$

where  $I$  is the original image,  $g(\cdot)$  is the camera response function (CRF),  $n_s$  is the irradiance-dependent noise component,  $n_c$  is the independent noise, and  $n_q$  is the additional quantization and amplification noise.

## 2 The Gaussian PSF

When the focus defect is considerable and diffraction effects are neglected, the geometrical optics approximation of the PSF of a defocused system corresponds to the pillbox function. Alternatively, some researchers have suggested using a 2D Gaussian in order to take into account the effects of polychromatic illumination, lens aberrations and other defects. At this point, it is worth asking if the Gaussian approximation is indeed a suitable model for a defocused system.

A thorough review of the literature reveals that the assumption of a Gaussian blur model has widely been accepted and exploited for different applications. One of its main advantages is its mathematical tractability derived from the properties of the Gaussian function. For instance, the Gaussian PSF has successfully been exploited in computer vision for depth retrieval through SFD

[24, 30], for proposing new focus measure operators [37], for computing the all-in-focus image in focus stacking [15, 1] and for image restoration and deblurring [6, 26, 22, 16, 7, 23]. The Gaussian PSF has also been exploited for assessing the effect of defocus blur in human depth perception [19]. Note, however, that some authors have opted for more general models when estimating the PSF of optical systems [31, 36, 14, 8, 13] or for accurately assessing human visual acuity [32, 35].

Previous researchers have shown that the geometrical approximation is similar to the exact, diffracted PSF for large amounts of defocus [28]. Notwithstanding, near the diffraction limit, the Gaussian PSF behaves as an all-pass filter, which neglects the limitations imposed by diffraction. A key aspect of the model proposed in the paper, is that the joint effect of the sampling function and diffraction can be replaced by an ideal low-pass filter. As a result, one can take advantage of the limited resolution of real imaging systems in order to derive an approximated model even at perfect focus. Note, however, that this approximation is not suitable for modeling the PSF of a defocused optical system and is, therefore, not suitable for some applications, such as image deblurring based on direct deconvolution.

### 3 Experiments in Shape-from-focus

This section provides experiments on the application of the proposed focus profile model for depth estimation using *shape-from-focus*.

Shape-from-focus can be divided into three main stages: focus measure, peak detection and post-processing. Once a focus sequence has been captured by changing focus, the *focus measure* stage consists of the application of a focus measure operator in order to compute the focus profile for each pixel of an imaged scene. Traditionally, *peak detection* has been performed by fitting a model,  $\tilde{\varphi}$ , to the measured focus profile,  $\varphi$ . The depth of the corresponding pixels is estimated by simply finding the maximum of the interpolated focus profile model. The obtained depth-map can be further improved by means of specific *post-processing* techniques that take into account the continuous nature of the imaged scene [29]. A wide variety of post-processing techniques have been proposed, including surface fitting and optimization by neural networks [4], and dynamic programming [2, 3], among many others (e.g., [27, 20, 18]).

Formally, the aim of SFF is to generate a depth-map,  $z(x, y)$ , whit the estimated depth at each  $(x, y)$  coordinate. For comparison purposes, the estimated depth has been computed using the Gaussian profile [21], the Laplacian-Cauchy profile [33, 20] and the proposed focus profile model. Since the aim of this experiment is to compare the different focus profile models, the presented results correspond to raw depth-maps without any post-processing stage.

In order to simplify the construction and measurement of the ground truth, the captured scenes mostly consisted of planar objects placed at different positions from the camera. For each scene, a focus sequence of 100 frames was acquired using a Sony SNC-RZ50P camera. The depth-map was then estimated

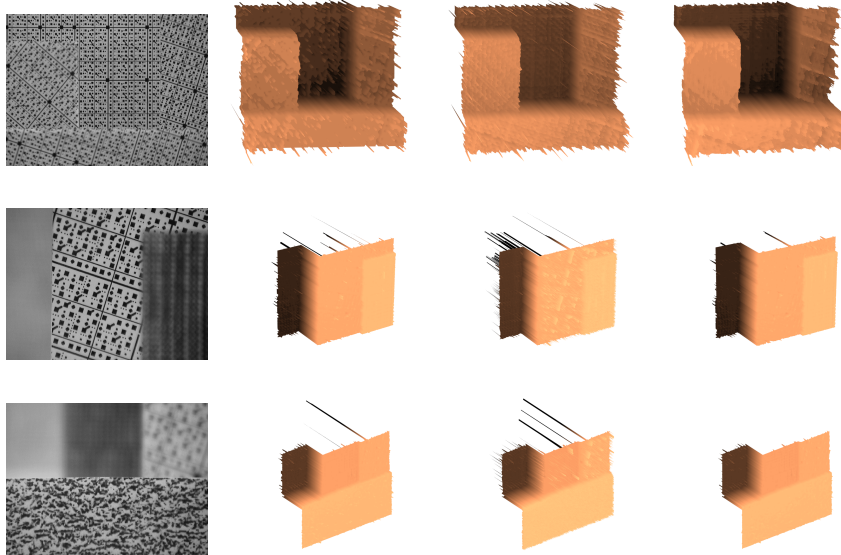


Figure 2: Performance of shape-from-focus using different focus profile models. From left to right: one frame of the focus sequence, Gaussian model, Laplacian-Cauchy model, and proposed model.

Table 1: Performance measures of SFF with different focus profile models: Gaussian [21], GP, Laplacian-Cauchy [20, 33], LC, and Proposed model, FP.

Method	RMSE	AE (%)	SNR (dB)	C
GP	0.108	1.52	35.9	0.972
LC	0.178	2.51	33.4	0.932
FP	<b>0.095</b>	<b>1.41</b>	<b>36.6</b>	<b>0.975</b>

by using SFF as described previously.

Five sequences have been used in the experiments and the depth-maps generated with different focus profile models have been compared. In order to measure the quality of the obtained depth-maps, the RMSE, the correlation (C), the signal-to-noise ratio (SNR), and the mean absolute error (AE) have been computed between the reconstructed depth-map,  $z(x, y)$ , and the ground truth,  $g_T(x, y)$ . Fig. 2 shows one frame of the focus sequence and the obtained depth-maps for three of the sequences used in the experiments. The mean results are summarized in Table 1. As shown in this table, the best performance of SFF is obtained when the proposed focus profile model is applied.

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